

Energy Implications of Economizer Use in California Data Centers

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Abstract

In the US, data center operations currently account for about 61 billion kWh/y of electricity consumption, which is more than 1.5% of total demand. Data center energy consumption is rising rapidly, having doubled in the last five years. A substantial portion of data-center energy use is dedicated to removing the heat generated by the computer equipment. Data-center cooling load might be met with substantially reduced energy consumption with the use of air-side economizers. This energy saving measure, however, has been shown to expose servers to an order-of-magnitude increase in indoor particle concentrations with an unquantified increase in the risk of equipment failure. An alternative energy saving option is the use of water-side economizers, which do not affect the indoor particle concentration but require additional mechanical equipment and tend to be less beneficial in high humidity areas. Published research has only presented qualitative benefits of economizer use, providing industry with inadequate information on which to base their design decisions. Energy savings depend on local climate and the specific building-design characteristics. In this paper, based on building energy models, we report energy savings for air-side and water-side economizer use in data centers in several climate zones in California. Results show that in terms of energy savings, air-side economizers consistently outperform water-side economizers, though the performance difference varies by location. Model results also show that conventional humidity restrictions must be relaxed or removed to gain the energy benefits of air-side economizers.

Introduction

Data centers are computing facilities that house the electronic equipment used for data processing, networking and storage. Rapid growth in computational demand emerging from various sectors of the economy is causing strong rates of increase in servers and IT-related hardware (IDC 2007). Server performance has doubled every two years since 1999, leading to increasingly higher densities of heat dissipation within data centers (Belady 2007). A substantial proportion of energy consumption in data centers is dedicated to the cooling load associated with electronic power dissipation (Tschudi et al. 2003). A recent study estimates that US data centers account for 61 billion kWh or 1.5% of the nation's annual electricity consumption (US DOE 2007a). This corresponds to an electricity bill of approximately \$4.5 billion in 2006 (EPA 2007). The environmental impact is substantial because 70% of the electricity in US is generated in power plants that burn fossil fuel (EIA 2007). Improved data center cooling technologies have the potential to provide significant energy savings. Cost savings and environmental benefits might also accrue.

A typical data center consists of rows of tall (2 m) cabinets or racks in which the servers, data storage and networking equipment are vertically arrayed. The cooling of data-center equipment is accomplished using computer room air conditioners (CRACs), which supply cold air to a raised-floor plenum beneath the racks. The CRAC system air handler is placed on the data center floor while chilled water is transported from compressor-based chillers to the CRAC cooling coils. More efficient cooling systems employ low outside air temperatures to reduce chiller load. Cooling towers that use ambient air to directly cool or precool the chilled water are known as water-side or fluid-side economizers. This type of system has been claimed to cut cooling-energy costs by as much as 70% (ASHRAE HVAC Fundamentals Handbook 2005) during economizer operation. Based on local weather data in San Jose, water-side economizers can be used for more than one-third of the year (PG&E 2006). An alternate data center arrangement uses air-handling units (AHU) and an air-side economizer. Such systems directly provide outdoor air for cooling whenever the temperature of outside air is lower than the set-point for return-air temperature in the data center. In San Francisco's cool climate, outside air could contribute to some level of air-side cooling for nearly all hours of the year (Syska Hennessy 2007). The use of air-side economizers brings with it an associated concern about contamination including moisture from humidity that may possibly threaten equipment reliability. Deliquescent sulfate, nitrate and chloride salts, in a humid environment (> 40% relative humidity) can cause corrosion, accumulate and become conductive, and may lead to electrical short-circuiting (Rice et al. 1981; Sinclair et al. 1990; Litvak et al. 2000). In this paper, the energy implications of a data center using a CRAC system will be compared with alternative cooling systems using air-side or water-side economizers for five different California climate zones. The modeling results and discussion focus on understanding the energy implications for both type of economizers and their effectiveness in different climate zones. The equipment reliability concerns associated with air-side economizers are acknowledged to be important, but addressing it is beyond the scope of the present paper.

Methods

Data center design scenarios

Energy-use simulations were performed for three different data center HVAC design scenarios (Figure 1). The baseline case considers a data center using conventional "computer room air conditioning" (CRAC) units. In this scenario, CRAC units are placed directly on the computer room floor. Air enters the top of a CRAC unit, passes across the cooling coils, and is then discharged to the underfloor plenum. Perforations in the floor tiles in front of the server racks allow the cool air to exit from the plenum into the data-center room. Fans within the computer servers draw the conditioned air upward and through the servers to remove equipment-generated heat. After exiting the backside of the server housing, the warm air rises and is transported to the intake of a CRAC unit. Most air circulation in the baseline scenario is internal to the data center. A small amount of air is supplied through a rooftop AHU to positively pressurize the room and to supply outside air for occupants. Cooling is provided by a water-cooled chiller plant. Refrigerant in the chillers is used to cool water through heat exchangers at the evaporator. The chilled water is then piped to the CRAC units on the data center floor. Waste heat from the chiller refrigerant is removed by water through heat exchangers in the condenser. Condenser water is piped from the cooling towers, which cool the water through interaction with the outside air. This baseline design is common to most mid- to large-size data

centers (Tschudi et al. 2003; Rumsey 2005; Syska Hennessy 2007).

The water-side economizer (WSE) scenario assumes a CRAC unit layout similar to that of the baseline case, except that additional heat exchangers are installed between the condenser water in the cooling towers and the chilled water supplied to the CRAC units. Under appropriate weather conditions, the cooling towers can cool the condenser water enough to cool the chilled water in the CRAC units directly, without operating the chiller plant. The CRAC units and chiller plant are assumed to be the same as in the baseline scenario.

The air-side economizer scenario (ASE) requires a different type of air delivery than typically found in a data center with conventional CRAC units. AHUs are placed outside of the data center room, commonly on the rooftop, and air is then sent to and from the computer racks through ducts. A ducted air delivery system creates greater air resistance than a conventional CRAC unit layout, though this system better prevents cold and warm air from unintentionally mixing within the data center. When the outside air temperature is equal to or below the temperature of the air supplied to cool the server, the AHU can directly draw outside air into the data center and exhaust all of the return air after it has passed across the computer servers. The movement of 100% outside air through the system can require more fan energy than the baseline case, as the economizer design requires more ducting, which increases air resistance through the system. However, during this 100% outside air mode the cooling is provided without operating the chiller, chilled water pumps, condenser water pumps, or the cooling tower fans. Outside air is also provided instead of recirculated air whenever the outside air temperature is greater than the supply air temperature but lower than that of the return air. Under this condition the chiller must operate, but the cooling required of the chiller is less than in a case with complete recirculation.

Energy modeling protocol

For each design scenario, the model calculations assume a 30,000 ft² (2800 m²) data center with an internal heat density of approximately 80 W/ft² (0.86 kW/m²; 2.4 MW total). This size and power density are characteristic of data centers evaluated in previous studies (Shehabi et al. 2008; Greenberg et al. 2006; Tschudi et al. 2003). The size of data centers varies greatly; 30,000 ft² is within the largest industry size classification, which is responsible for most servers in the US (IDC 2007). Power density in data centers is rapidly increasing (Uptime Institute 2000) and a power density of 80 W/ft² is currently considered to be of low- to mid-range (Rumsey 2008).

Basic properties of the modeled data center for all three scenarios are summarized in Table 1. Energy demand is calculated as the sum of the loads generated by servers, chiller use, fan operation, transformer and uninterruptible power supply (UPS) losses, and building lighting. The chiller encompasses coolant compressor, chilled water pumps, condensing water pumps, humidification pumps, and cooling-tower fans. Energy demand for servers, UPS, and lighting are constant, unaffected by the different design scenarios, but are included to determine total building-energy use. The base case and WSE scenarios assume conventional humidity restrictions recommend by ASHRAE (ASHRAE 2005). The ASE scenario assumes no humidity restriction, which is an adjustment required to gain ASE benefits as is typical in ASE implementation (Rumsey 2008). Air-side economizers also require a different air distribution design and the fan parameters associated with each design scenario are listed in Table 2. The

properties of other pumps and fans throughout the HVAC system remain constant for all three scenarios. Values are from previous data-center energy analyses (Rumsey 2008; Rumsey 2005).

The energy modeling approach used in this study applies a previously used protocol (Rumsey 2008; Rumsey 2005) and is based on a combination of fundamental HVAC sizing equations that apply equipment size and efficiencies observed through professional experience. Building energy modeling is typically performed using energy models such as DOE-2, which simultaneously models heat sources and losses within the building and through the building envelope. However, models such as DOE-2 are not designed to incorporate some of the HVAC characteristics unique to data centers. Also, data centers have floor-area-weighted power densities that are 15-100 times higher than those of typical commercial buildings (Greenberg et al. 2006). This allows accurate modeling of data-center energy use to focus exclusively on internal heat load and the thermal properties of outdoor air entering the building. This is the approach taken in this study, as heat generated from data center occupants and heat transfer through the building envelope are negligible relative to the heat produced by servers. The building envelope may influence the cooling load in low-density data centers housed in older buildings that have minimal insulation. Evaluating this building type is worthy of exploration, but the required analysis is more complex and outside the scope of the present paper.

Both air-side and water-side economizers are designed to allow the chiller to shut down or reduce chiller energy load under appropriate weather conditions. Less overall energy is required for operation when the chiller load is reduced, but chiller efficiency is compromised. Changes in chiller efficiency used in this analysis are shown in Figure 2, representing a water-cooled centrifugal chiller with a capacity > 300 tons and condenser water temperature of 80 °F. A chilled water temperature of 45 °F, which is standard practice for data center operation, is used in the base case and ASE scenario. The WSE scenario uses a chilled water temperature of 52 °F, which is common when using water-side economizers. This increases needed airflow rates but allows greater use of the water-side economizers. The curves are based on the DOE2.1E software model and apply coefficients specified in the Nonresidential Alternative Calculation Method (ACM) Approval Manual for the 2005 Building Energy Efficiency Standards for Residential and Nonresidential Buildings (CEC 2005).

Annual data center energy use is evaluated for each of the three configuration scenarios assuming that a data center building is located in each of the five cities shown in Figure 3. Weather conditions at each city are based on hourly DOE2.1E weather data for California climate zones (CEC 2005).

Results and Discussion

Results from each scenario modeled are presented in Table 3 as a “performance ratio” which equals the ratio of total building energy divided by the energy required to operate the computer servers. Lower value of the performance ratio implies better energy utilization of the HVAC system. The performance ratio for the base case is 1.55 and, as expected, is the same for all the cities analyzed, since the operation of this design is practically independent of outdoor weather conditions. The base case performance ratio is better than the current stock of data centers in the US (EPA 2007; Koomey 2007) because the base case represents newer data centers with water-cooled chillers, which are more efficient than the air-cooled chillers and direct expansion (DX) cooling systems found in older data centers.

The performance ratios for the ASE and WSE scenarios show air-side economizers consistently provide savings relative to the base case, though the difference in savings between the two scenarios varies. It is important to note that even small changes in the performance ratio results in significant savings, given the large amount of energy used in data centers. For example, reducing the performance ratio at the model data center in San Jose from 1.55 to 1.44 represents a savings of about 1.9 million kWh/y, which corresponds to a cost savings of more than \$130,000/y (assuming \$0.07/kWh).

Figure 4 shows the disaggregation of the cooling systems' annual energy use, normalized by floor area, for each modeled data center by location and design scenario. The annual energy use dedicated to the servers, UPS, and lighting is 584, 95, and 9 kWh/ft², respectively. These energy values are independent of the climate and HVAC design in scenario and not included in the graphs in Figure 4. Economizer use is typically controlled by combination of outside air temperature, humidity, and enthalpy; however results shown in Figure 4 are for economizer use controlled by outside air temperature only. Results show that the ASE scenario provides the greatest savings in San Francisco while Fresno provides the least ASE savings. Sacramento benefited the most from the WSE scenario while minimal savings were realized in Los Angeles and San Francisco. The San Francisco WSE scenario, where significant gains would be expected because of the cool climate, is hindered by chiller part-load inefficiencies. The relatively higher moisture content in the San Francisco air increases the latent cooling load in the model and causes the chiller plant to reach the capacity limit of the first chiller more often, activating a second chiller. The second chiller shares the cooling load equally with the first, resulting in a transition from one chiller at a high load factor (efficient operation) to two chillers at slightly above half the load factor (less efficient operation). The results from the WSE scenario in San Francisco emphasize the need for engineers to model the hour-by-hour load, rather than just the peak load, and to size chillers such that all active chillers at any moment will be running near their most efficient operating point.

Figure 5 shows that removing the humidity restrictions commonly applied to data centers is necessary to gain ASE energy savings. As the relative humidity (RH) range is narrowed, energy use from the fans begins to sharply increase, surpassing the equivalent baseline energy in most of the cities. Humidity levels are often restricted in data centers to minimize potential server reliability issues. ASHRAE's guidelines released in 2005 for data centers provide a "recommend" RH range between 40-55% and an "allowable" range between 20-80% (ASHRAE 2005). There is minimal cost in applying the more conservative ASHRAE RH restrictions in conventional data center design, such as the baseline in this study shown in Figure 5. The influence of humidity on server performance, however, is poorly documented and the need for humidity restrictions is increasingly being questioned (Fontecchio 2007). The energy saving difference between adhering to ASHRAE's recommend RH range versus the allowable RH range is substantial, and warrants further investigation.

Conclusion

Employing the energy-saving measures evaluated in this paper would require a shift in conventional data center design and operation. Various operational concerns must be addressed before widespread adoption of these technologies could be expected in data-center buildings. This paper contributes to the informed implementation of air-side and water-side economizers by assessing the energy benefits of adopting these efficiency improvements. Air-side economizers

are shown to consistently outperform water-side economizers in California, though the difference in performance varies by the climate conditions of the locations evaluated. Furthermore, the models show that conventional humidity restrictions must be relaxed or removed to substantially realize the energy benefits of air-side economizers. As the data center economy continues to rapidly grow, energy efficiency will continue to emerge as an important financial and environmental concern. The results presented here contribute to our understanding of different design implications and should assist decision makers in the implementation of energy-efficient data centers.

Acknowledgments

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Table 1: Data Center Characteristics Common to All Design Scenarios

Data Center Parameters	
Floor Area	30,000 ft ²
UPS Waste Heat	326 kW
Data Center Lights	30 kW
Total Rack Load	2000 kW
Total Internal Load	2,356 kW
Average Internal Load Density	79 W/ft ²
Minimum Ventilation	4,500 ft ³ /min
Supply Air Temperature	55 °F
Return Air Drybulb Setpoint	72 °F
Chiller Capacity	1750 kW
Number of Chillers	3

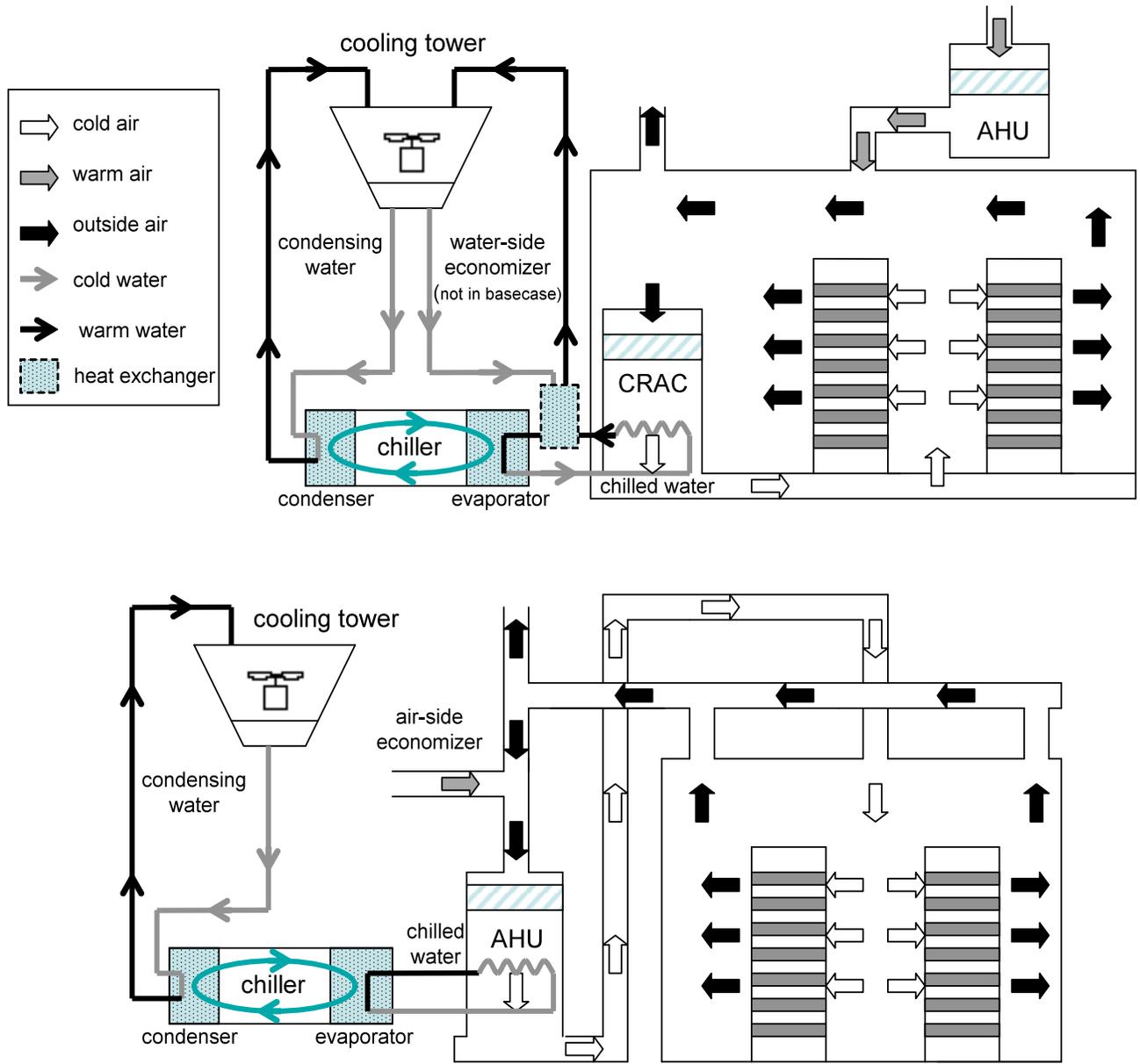
Table 2: Data Center Fan Properties

Fan System Parameters	Baseline and WSE			ASE	
	MU AH	Exhaust	CRAC s	Supply	Relief
Total Air Flow (cfm)	4,500	4,500	495,000	437,758	437,758
Fan Motor Size, Nominal (hp)	7.5	3	10	30	50
Number of Fans	1	1	30	10	5
Fan Efficiency	53.3%	44.0%	55.6%	63.8%	67.5%
Fan Drive Efficiency	95%	95%	95%	95%	95%
Fan Motor Efficiency	89.6%	86.2%	90.1%	92.5%	93.2%
VFD Efficiency	n/a	n/a	n/a	98%	98%
Total Static Pressure Drop (in.w.g.)	3.5	1	1.6	2	1

Table 3: Ratio of Total Building Energy to Computer Server Energy

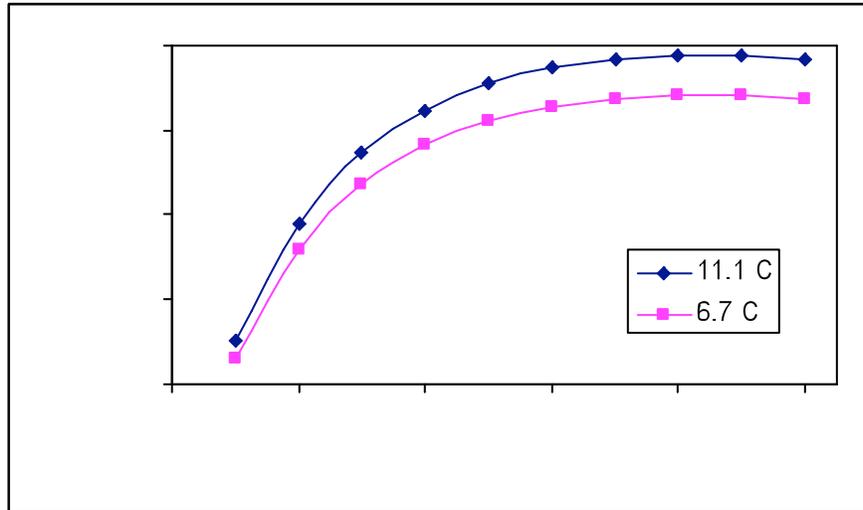
	San Jose	San Francisco	Sacramento	Fresno	Los Angeles
Baseline	1.55	1.55	1.55	1.55	1.55
Air-side Economizer	1.44	1.42	1.44	1.46	1.46
Water-side Economizer	1.53	1.54	1.53	1.53	1.54

Figure 1: Schematic of Data Center Cooling Design Scenarios



Air and water flow schematic for the basecase and water-side economizer scenarios (above).
 Air and water flow schematic for the air-side economizer scenario (below).

Figure 2: Assumed Part Load Performance of Data Center Chillers



Part load efficiencies for a water-cooled centrifugal chiller with a capacity >300 tons and an condenser water temperature of 26.7 °C (CEC, 2005)

Figure 3: Evaluated Climate Zone Locations

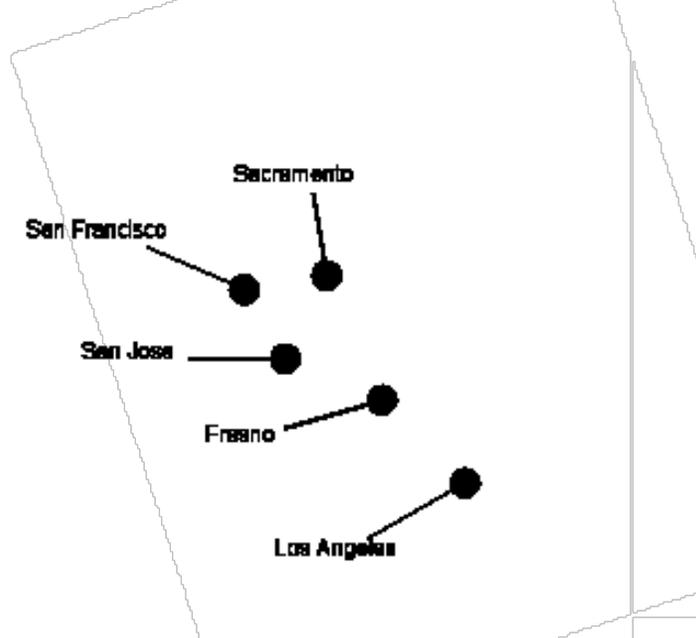


Figure 4: Disaggregated Energy Use (Climate Dependent Values Only)

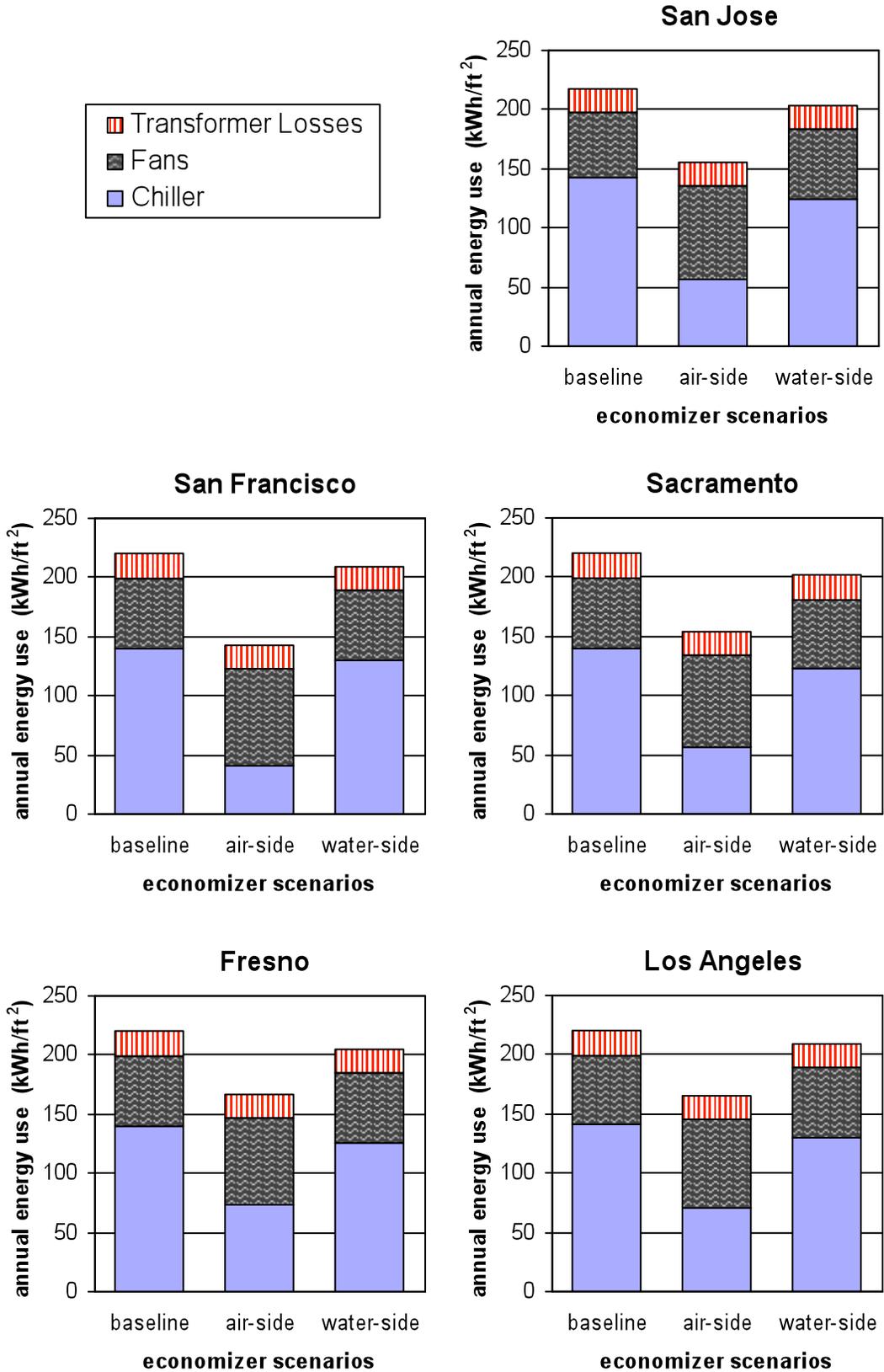


Figure 5: Chiller and Fan Energy Resulting from Humidity Restrictions

